

Moveout approximations for P waves in media of monoclinic and higher anisotropy symmetries

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Outline

Introduction

Traveltime approximations

Normal moveout velocity

Tests of the formulae

Conclusions

Introduction

Moveout approximations

standard

- expansion of T^2 in terms of the squared offset

hyperbolic, non-hyperbolic, ...

alternative

- expansion of T^2 in terms of the deviations

of anisotropy from isotropy

Introduction

Monoclinic or higher symmetry anisotropic media

Unconverted P wave

reflected from a plane reflector Σ

coinciding with a symmetry plane

\Rightarrow ray of reflected P wave in a plane \perp reflector Σ

2D problem in the (x', z') plane of local x', y', z' coordinate system

Two-step derivation: 1) local, 2) global coordinates

Traveltime approximations

Normal moveout formula

$$T^2(x) = (4H^2 + x^2)/v^2(\mathbf{n})$$

$T(x)$ - traveltime at the offset x

$v(\mathbf{n})$ - ray velocity; the same on down- and up-going leg of ray

\mathbf{n} - unit vector in the direction of the slowness vector

\mathbf{n} may deviate from (x', z') plane

H - depth of the plane reflector

Travelttime approximations

Normalized moveout formula

$$\bar{x} = x/2H , \quad T_0 = 2H/\alpha_0$$

$$T^2(\bar{x}) = \alpha_0^2 T_0^2 (1 + \bar{x}^2)/v^2(\mathbf{n})$$

T_0 - two-way zero-offset travelttime

\bar{x} - normalized offset

α_0 - vertical velocity ($\alpha_0^2 = A_{33}$)

$A_{\alpha\beta}$ - density-normalized elastic moduli in the Voigt notation

Traveltime approximations

Problem: Needed: $v^2(\mathbf{n})$

Available: \mathbf{N} and $c^2(\mathbf{N})$

$c(\mathbf{N})$ - phase velocity

$v(\mathbf{n})$ - ray velocity

\mathbf{n} - unit vector in the direction of the slowness vector

\mathbf{N} - unit vector in the direction of the ray-velocity vector \mathbf{v}

\Rightarrow need to find the relation between $v^2(\mathbf{n})$ and $c^2(\mathbf{N})$

Traveltime approximations

Approximations of ray velocity

1) Ignore the difference between \mathbf{n} and \mathbf{N}

$$v^2(\mathbf{n}) = c^2(\mathbf{N})$$

2) Consider the difference between \mathbf{n} and \mathbf{N}

$$v^2(\mathbf{n}) = (c^4(\mathbf{N}) - 4[B_{13}^2(\mathbf{N}) + B_{23}^2(\mathbf{N})])/c^2(\mathbf{N})$$

3) Consider the difference between \mathbf{n} and \mathbf{N}

and use 2nd-order approximation of c

$$v^2(\mathbf{n}) = (c^4(\mathbf{N}) + 4a[B_{13}^2(\mathbf{N}) + B_{23}^2(\mathbf{N})])/c^2(\mathbf{N})$$

Traveltime approximations

Approximations of ray velocity

$$B_{13}(\mathbf{N}) = \alpha_0^2 N'_1 N'_3 [\delta'_y - 2(\delta'_y - \epsilon'_x) N_1'^2]$$

$$B_{23}(\mathbf{N}) = \alpha_0^2 N'_1 (\chi'_z N_3'^2 + \epsilon'_{16} N_1'^2)$$

$$c^2(\mathbf{N}) = B_{33}(\mathbf{N}) = \alpha_0^2 (1 + 2N_1'^2 [\epsilon'_x + (\delta'_y - \epsilon'_x) N_3'^2])$$

$$a = (r^2 - 3/4)/(1 - r^2) \quad r = \beta_0/\alpha_0 \quad \beta_0^2 = A_{55}$$

$\epsilon'_x, \delta'_y, \chi'_z, \epsilon'_{16}$ - WA parameters in local coordinate system

N'_i - components of \mathbf{N} in local coordinate system ($N'_2 = 0$)

Traveltime approximations

Traveltime formulae - local coordinates

$$1) T^2(\bar{x}) = T_0^2 ((1 + \bar{x}^2)^3)/P(\bar{x})$$

$$2) T^2(\bar{x}) = T_0^2 (P(\bar{x})(1 + \bar{x}^2)^3)/(P^2(\bar{x}) - Q_1^2(\bar{x}) - (1 + \bar{x}^2)Q_2^2(\bar{x}))$$

$$3) T^2(\bar{x}) = T_0^2 (P(\bar{x})(1 + \bar{x}^2)^3)/(P^2(\bar{x}) + a[Q_1^2(\bar{x}) + (1 + \bar{x}^2)Q_2^2(\bar{x})])$$

$$P(\bar{x}) = (1 + \bar{x}^2)^2 + 2\delta'_y \bar{x}^2 + 2\epsilon'_x \bar{x}^4$$

$$Q_1(\bar{x}) = 2\bar{x}[2\epsilon'_x \bar{x}^2 + \delta'_y(1 - \bar{x}^2)] \quad Q_2(\bar{x}) = 2\bar{x}(\chi'_z + \epsilon'_{16} \bar{x}^2)$$

Normal moveout velocity

Definition

$$v_{NMO}^{-2} = dT^2/dx^2|_{x=0}$$

Local coordinates

$$1) v_{NMO}^{-2} = \alpha_0^{-2}(1 - 2\delta'_y)$$

$$2) v_{NMO}^{-2} = \alpha_0^{-2}[1 - 2\delta'_y + 4((\delta'_y)^2 + (\chi'_z)^2)]$$

$$3) v_{NMO}^{-2} = \alpha_0^{-2}[1 - 2\delta'_y - 4a((\delta'_y)^2 + (\chi'_z)^2)]$$

Normal moveout velocity

Global coordinates

$$v_{NMO}^{-2} = W_{11} \cos^2 \varphi + 2W_{12} \cos \varphi \sin \varphi + W_{22} \sin^2 \varphi$$

$$1) W_{11} = \alpha_0^{-2}(1 - 2\delta_y) \quad W_{12} = -2\alpha_0^{-2}\chi_z \quad W_{22} = \alpha_0^{-2}(1 - 2\delta_x)$$

$$3) W_{11} = \alpha_0^{-2}[1 - 2\delta_y - 4a(\delta_y^2 + \chi_z^2)] \quad W_{12} = -2\alpha_0^{-2}\chi_z[1 + 2a(\delta_x + \delta_y)]$$

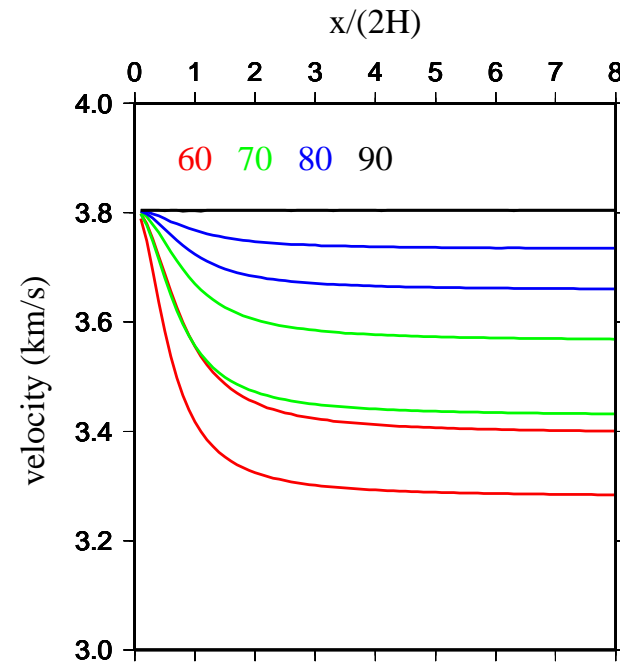
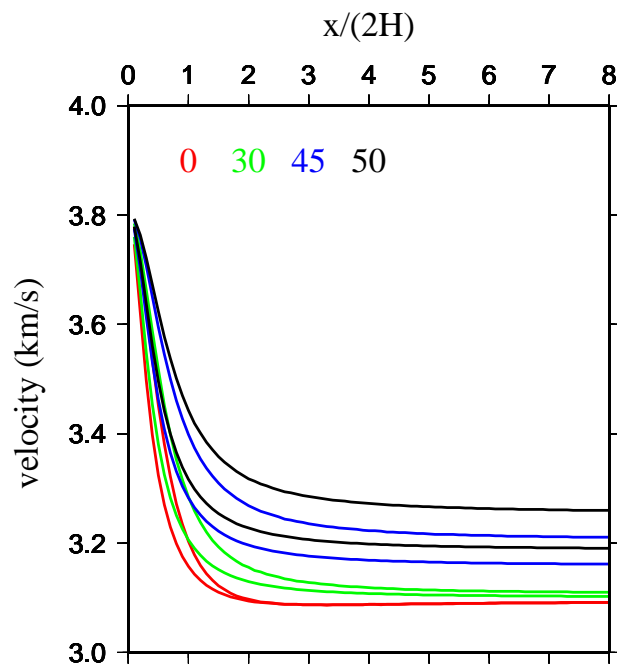
$$W_{22} = \alpha_0^{-2}[1 - 2\delta_x - 4a(\delta_x^2 + \chi_z^2)]$$

φ - angle of the source-receiver profile with x -axis

Tests of the formulae

HTI model, anisotropy $\sim 26\%$

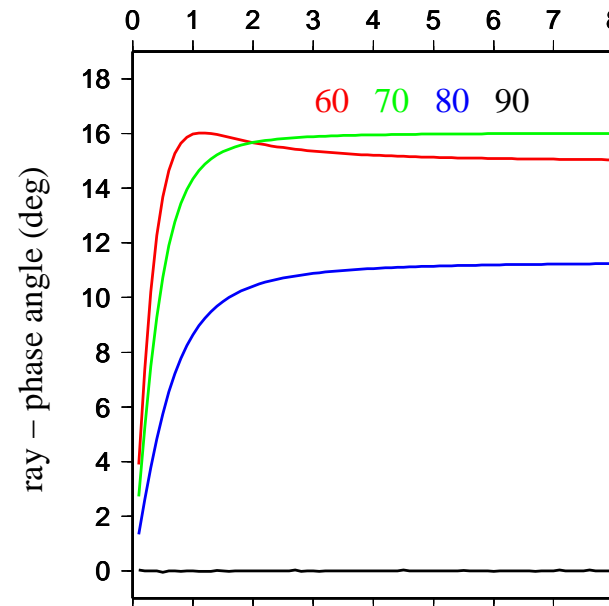
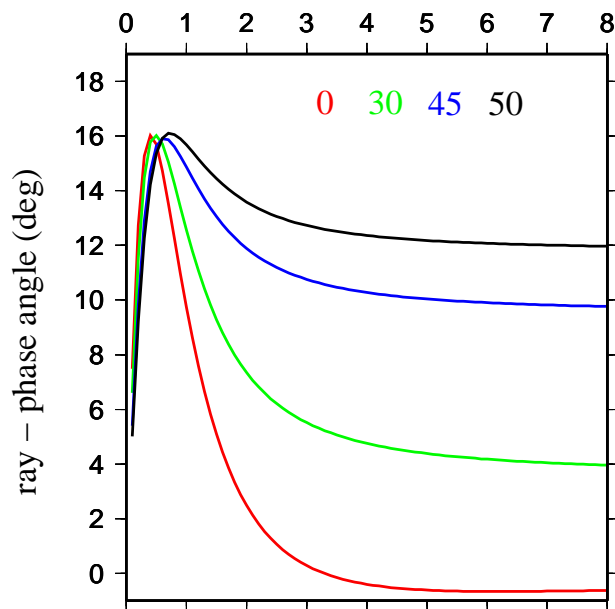
$$\alpha_0=3.805 \text{ km/s}, \quad \beta_0=1.510 \text{ km/s}, \quad \epsilon_x=-0.169, \quad \delta_y=-0.373$$



Tests of the formulae

HTI model, anisotropy $\sim 26\%$

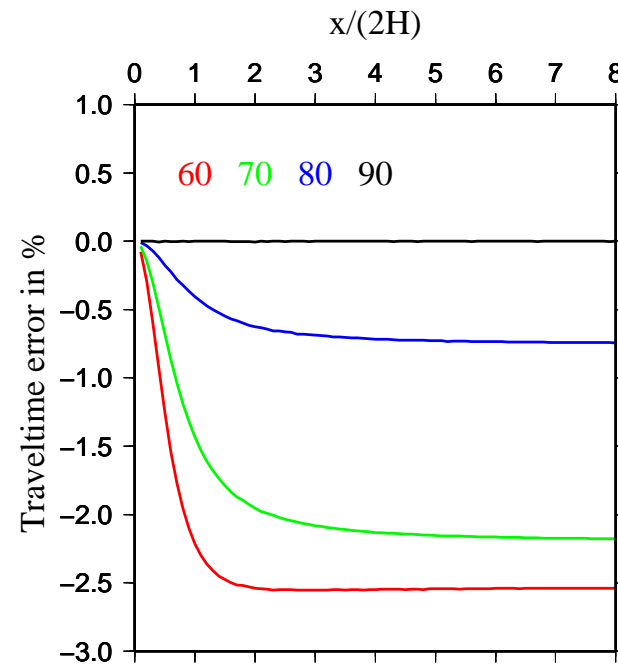
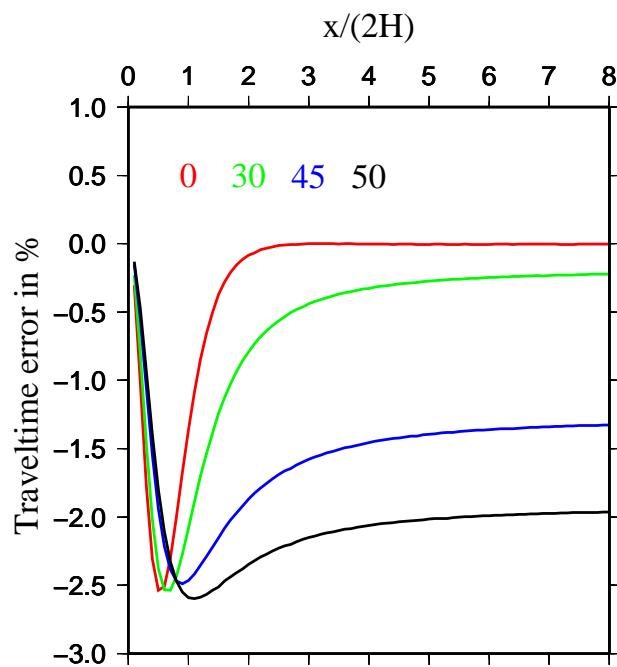
$\alpha_0=3.805$ km/s, $\beta_0=1.510$ km/s, $\epsilon_x=-0.169$, $\delta_y=-0.373$



Tests of the formulae

HTI model, anisotropy $\sim 26\%$, formula # 1

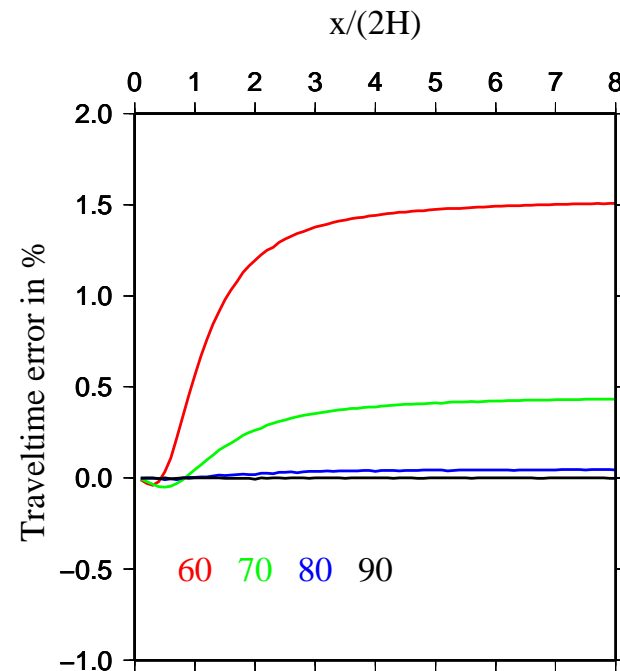
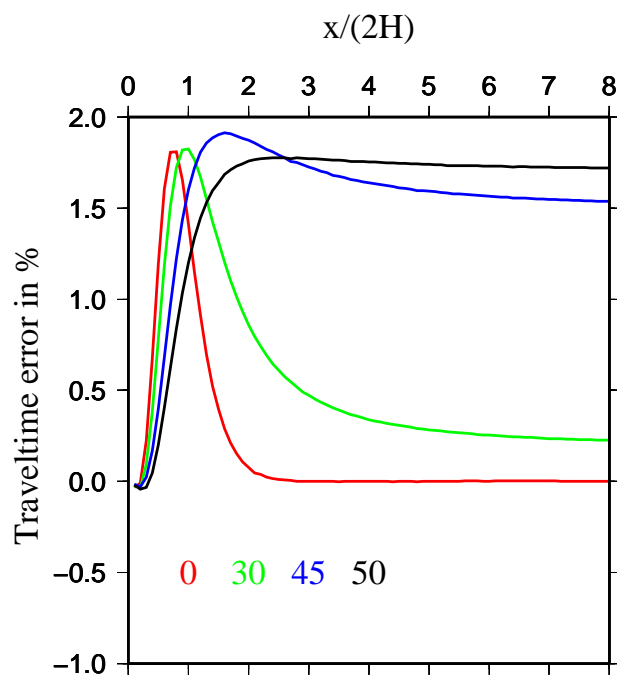
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Tests of the formulae

HTI model, anisotropy $\sim 26\%$, formula # 2

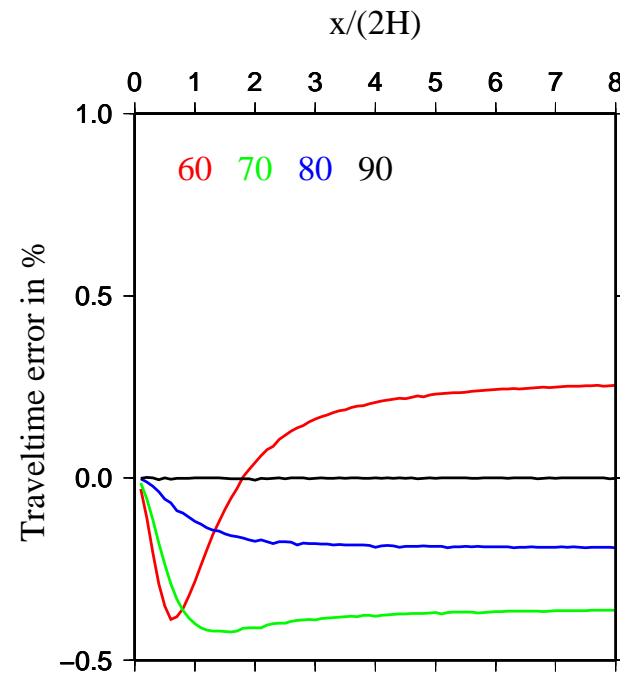
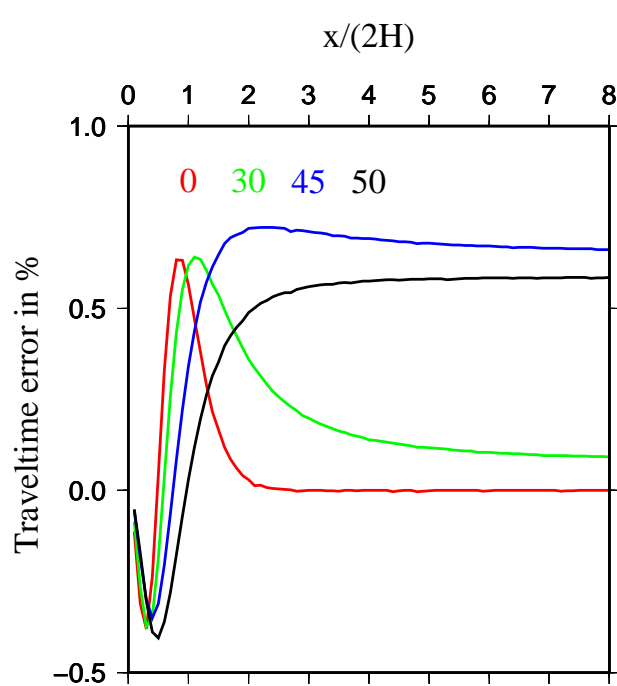
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Tests of the formulae

HTI model, anisotropy $\sim 26\%$, formula # 3

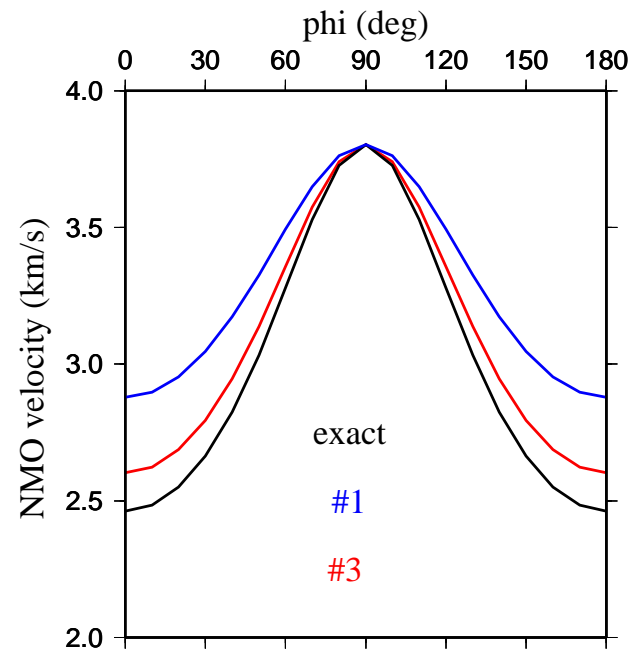
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Tests of the formulae

HTI model, anisotropy $\sim 26\%$

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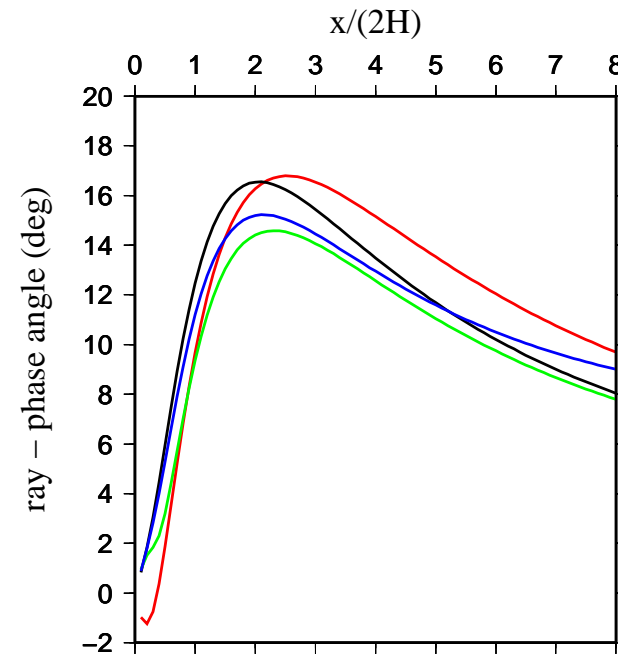
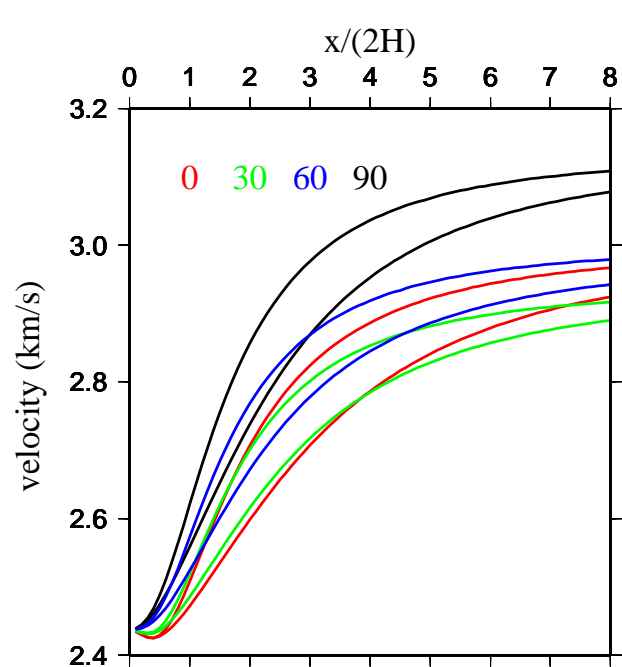


Tests of the formulae

ORT model, anisotropy $\sim 25\%$

$$\alpha_0=2.437 \text{ km/s}, \quad \beta_0=1.414 \text{ km/s}, \quad \epsilon_x=0.258, \quad \epsilon_y=0.328$$

$$\delta_x=0.077, \quad \delta_y=-0.083, \quad \delta_z=0.340$$

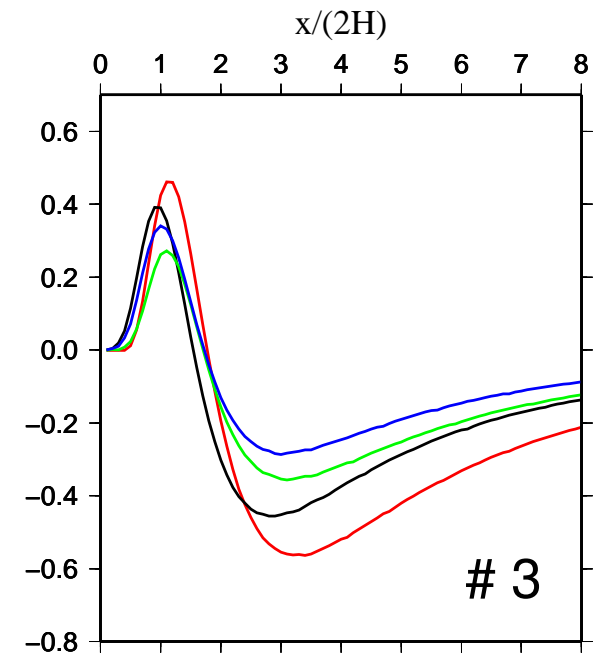
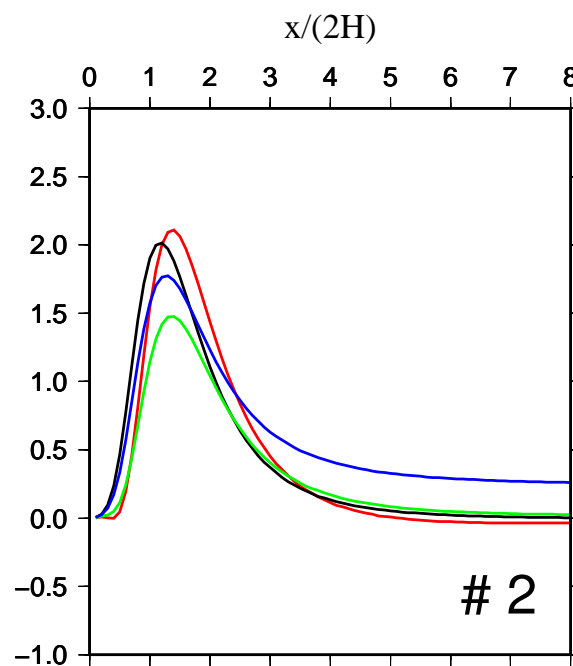
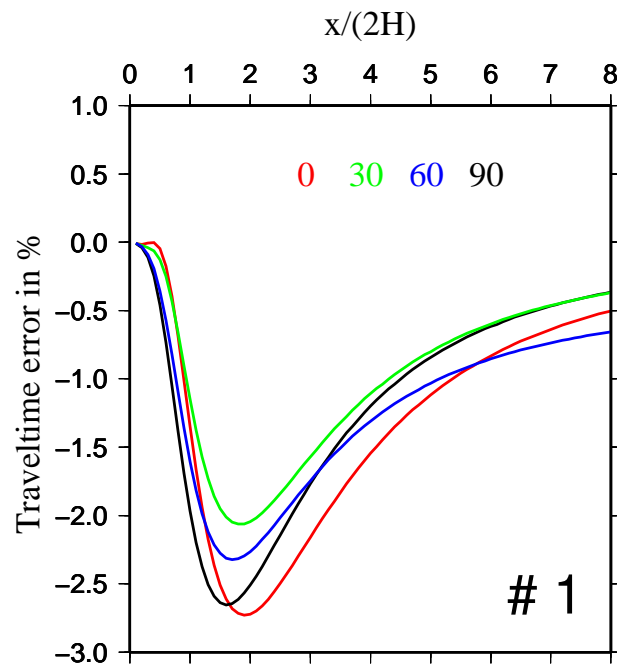


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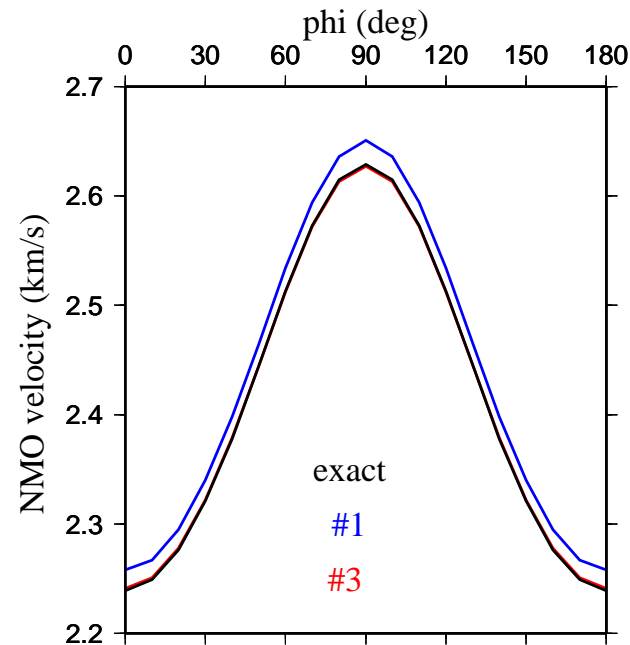


Tests of the formulae

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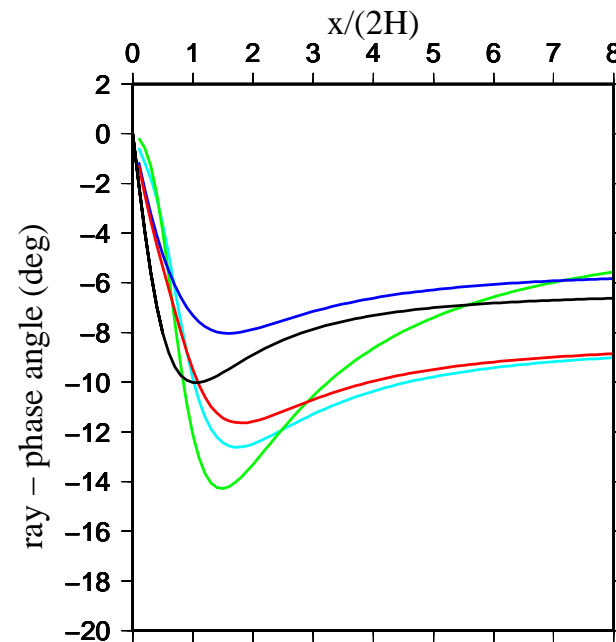
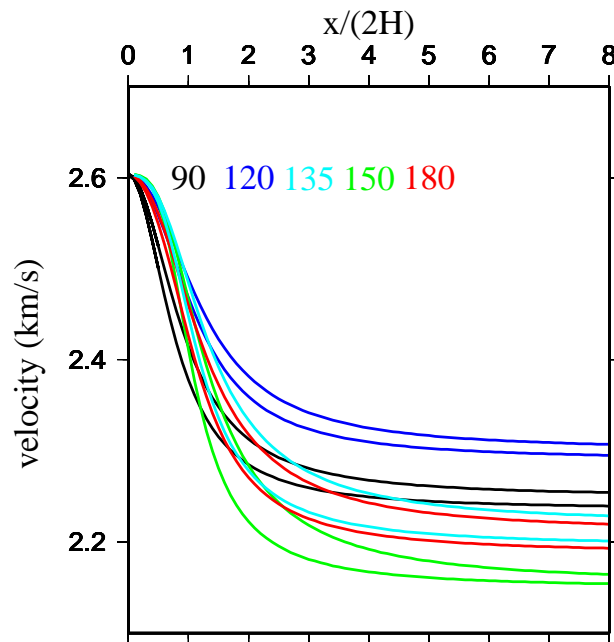
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Tests of the formulae

MONO model, anisotropy $\sim 15\%$

$\alpha_0=2.604$ km/s, $\beta_0=1.566$ km/s, $\epsilon_x=-0.135$, $\epsilon_y=-0.124$, $\delta_x=-0.128$,
 $\delta_y=-0.057$, $\delta_z=-0.241$, $\epsilon_{16}=0.057$, $\epsilon_{26}=-0.043$, $\chi_z=-0.071$

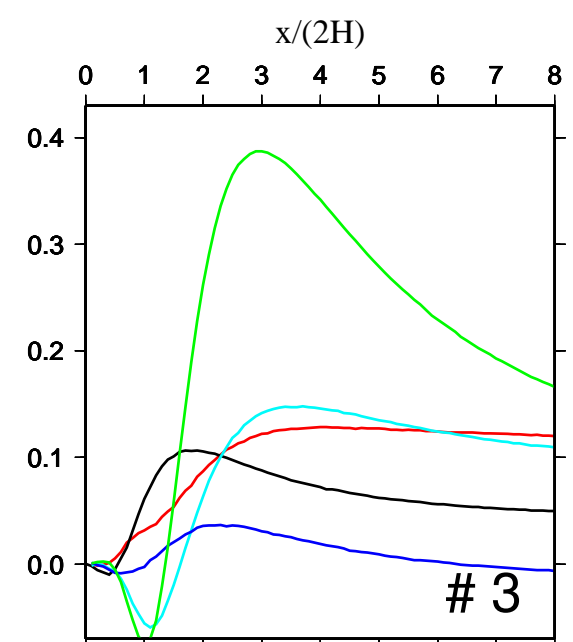
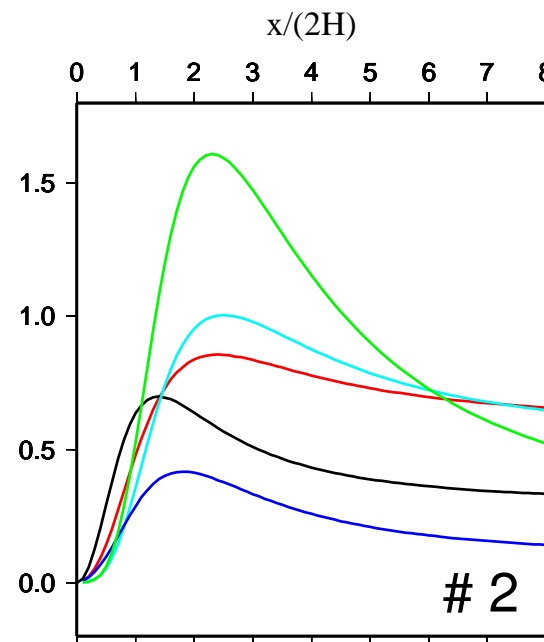
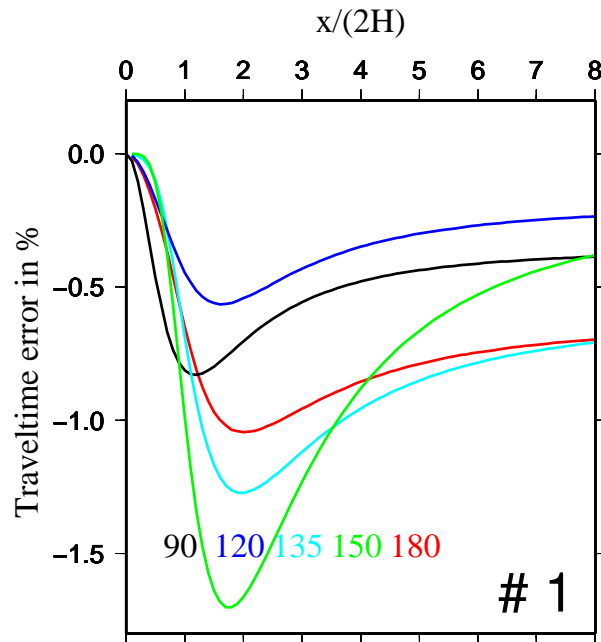


Tests of the formulae

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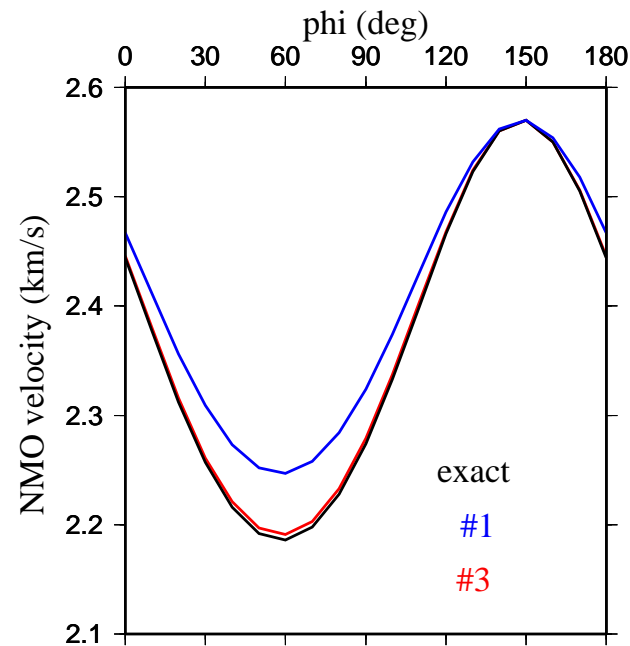
$\delta_y=-0.057$, $\delta_z=-0.241$, $\epsilon_{16}=0.057$, $\epsilon_{26}=-0.043$, $\chi_z=-0.071$



Tests of the formulae

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Conclusions

- based on WA approximation
- relatively simple formulae; no non-physical assumptions
- applicable to VTI, HTI, orthorhombic or even monoclinic media
for their reflector || with a plane of symmetry
- inaccuracies for large deviations of \mathbf{n} and \mathbf{N}
- for small and large offsets accurate
- second-order formulae very accurate; $< 1\%$ for $\sim 25\%$ anisotropy
- reduced number of WA parameters (WA/exact):
monoclinic - 8/12, orthorhombic - 5/9, TI - 2/4
- byproduct: simple expressions for NMO velocities

Generalizations

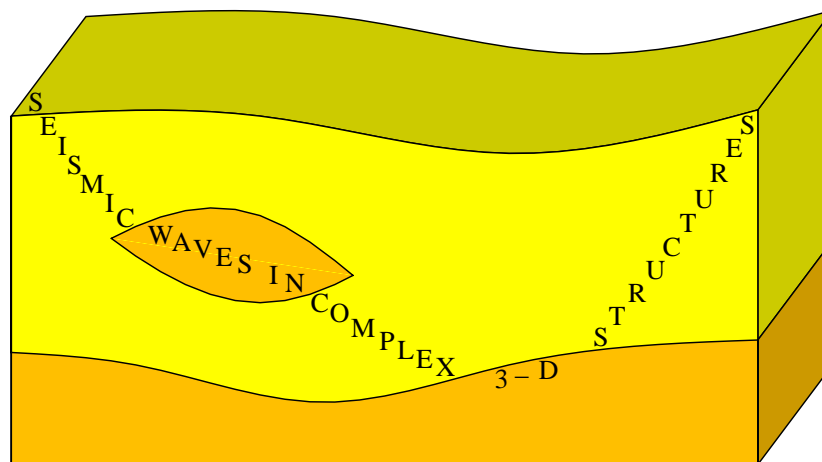
Straightforward

- dip-constrained media with an inclined reflector
parallel to a symmetry plane
- unconverted coupled S wave along a common ray

Possible

- converted waves

Acknowledgements



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